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Electromagnetic fields of charged beams in gradually tapering waveguides

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MOPNET 3

Heriot-Watt University

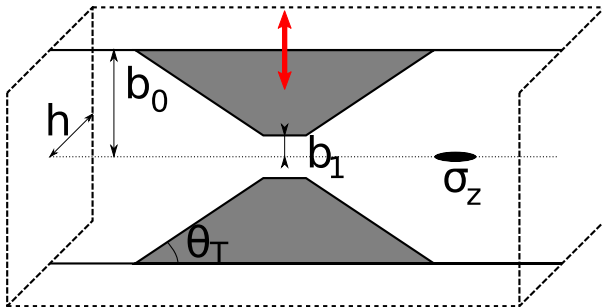
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¹University of the Highlands and Islands, Scotland

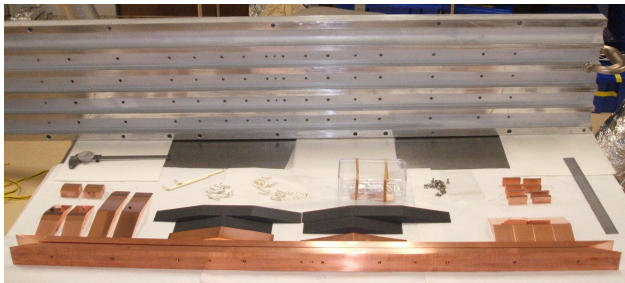
Examples of non-uniform metallic structures in accelerators :

- ▶ collimators



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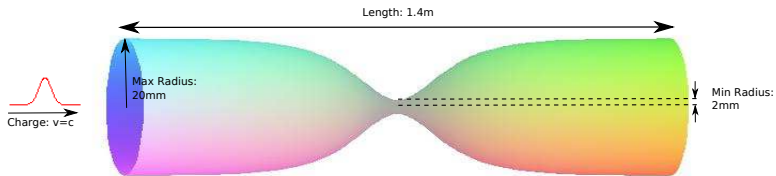




Motivation

Examples of non-uniform metallic structures in accelerators :

- ▶ transition between subsystems, e.g. beam pipe in a small gap undulator





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Challenge

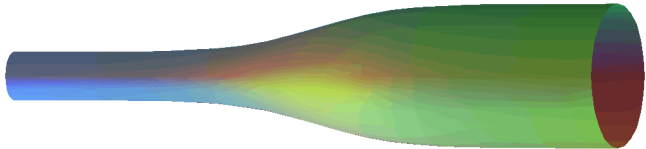
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 - ▶ induces instabilities in the particle beam, and destroys its useful properties



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 - ▶ induces instabilities in the particle beam, and destroys its useful properties
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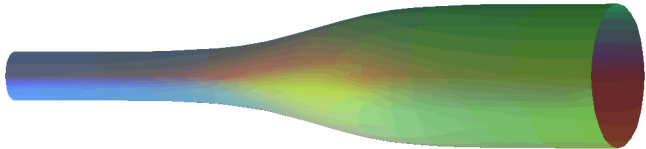




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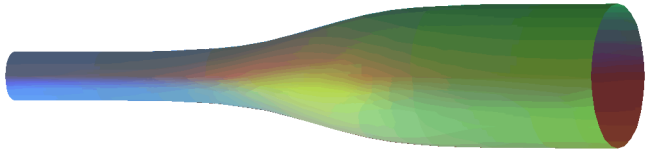
- ▶ Slow variation \implies computationally intensive



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- ▶ Slow variation \implies computationally intensive
- ▶ BUT slow variation \implies amenable to analytical methods
 - ▶ (practical limitations : size of tunnel and resistance of the structure)



Electromagnetic 2-form

- ▶ Electromagnetic 2-form F is related to \mathbf{E} and \mathbf{B} as follows :

$$F = dt \wedge (E_x dx + E_y dy + E_z dz) \\ - B_x dy \wedge dz - B_y dz \wedge dx - B_z dx \wedge dy \quad (1)$$

- ▶ Perfect conductor boundary condition at $\mathcal{S} = 0$

$$d\mathcal{S} \wedge F = 0 \Big|_{\mathcal{S}=0} \quad (2)$$

is equivalent to $\mathbf{n} \times \mathbf{E} = 0$ and $\mathbf{n} \cdot \mathbf{B} = 0$ where \mathbf{n} is normal to \mathcal{S}

Maxwell's equations

- ▶ Maxwell's equations

$$dF = 0, \quad \varepsilon_0 d \star F = -\varrho \star \tilde{V} \quad (3)$$

where ϱV is the electric 4-current of the particle beam



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- ▶ for an unperturbed beam

$$V = \frac{1}{c} \frac{\partial}{\partial t} + \frac{\partial}{\partial z} \quad (4)$$

assuming that it is travelling close to the speed of light c



Potential decomposition

- ▶ Exploit cylindrical symmetry of waveguide :

$$\begin{aligned} F = & \left(\partial_u \mathcal{H}^\phi + \partial_u \mathcal{H}^B + \partial_\zeta \mathcal{H}^B - 2\partial_{u\zeta}^2 W - \partial_{\zeta\zeta}^2 W \right) d\zeta \wedge du \\ & + du \wedge \left[d_\perp \left(\partial_u W + \partial_\zeta W - \mathcal{H}^B \right) + \partial_u \#_\perp d_\perp X \right] \\ & + d\zeta \wedge \left[d_\perp \left(\mathcal{H}^B - \partial_\zeta W \right) + \#_\perp d_\perp \left(\partial_\zeta X - \mathcal{H}^\varphi \right) \right] \\ & + \left(\partial_\zeta \mathcal{H}^\varphi + \partial_u \mathcal{H}^\phi + \mathcal{H}^b - 2\partial_{u\zeta}^2 X - \partial_{\zeta\zeta}^2 X \right) \#_\perp 1 \end{aligned} \quad (5)$$

where $\zeta = z$, $u = z - ct$, d_\perp is the exterior derivative acting in the (x, y) subspace (transverse subspace) and $\#_\perp$ is the Hodge map on the transverse subspace

- ▶ Follows from Hodge decomposition

$\Lambda_1(\mathcal{D}) = d_\perp \mathcal{F}_d(\mathcal{D}) \oplus \#_\perp d_\perp \mathcal{F}(\mathcal{D})$ on the transverse cross-section \mathcal{D} of the waveguide



Field equations

Maxwell's equations may be reduced to :

$$\delta_{\perp} d_{\perp} \mathcal{H}^B = 0, \quad (6)$$

$$d_{\perp} \mathcal{H}^b = \#_{\perp} d_{\perp} \left(\partial_u \mathcal{H}^B \right), \quad (7)$$

$$d_{\perp} \mathcal{H}^{\varphi} = \#_{\perp} d_{\perp} \mathcal{H}^{\Phi}, \quad (8)$$

$$\begin{aligned} \delta_{\perp} d_{\perp} W - 2\partial_{u\zeta}^2 W - \partial_{\zeta\zeta}^2 W \\ + \partial_u \mathcal{H}^{\Phi} + \partial_u \mathcal{H}^B + \partial_{\zeta} \mathcal{H}^B = P(r, \theta, u), \end{aligned} \quad (9)$$

$$\delta_{\perp} d_{\perp} X - 2\partial_{u\zeta}^2 X - \partial_{\zeta\zeta}^2 X + \partial_{\zeta} \mathcal{H}^{\varphi} + \partial_u \mathcal{H}^{\varphi} + \mathcal{H}^b = 0 \quad (10)$$

where $\delta_{\perp} d_{\perp}$ is the transverse Laplacian and

$$\partial_u P(r, \theta, u) = \rho(r, \theta, u)$$

Boundary conditions

Cylindrical symmetry with \mathcal{S} as $r = R(\zeta)$:

$$W = 0|_{r=R(\zeta)}, \quad (12)$$

$$\partial_r X = 0|_{r=R(\zeta)}, \quad (13)$$

$$\mathcal{H}^B = \partial_\zeta W|_{r=R(\zeta)}, \quad (14)$$

$$\mathcal{H}^\Phi = -R'(\zeta) \frac{1}{r} \partial_\theta X|_{r=R(\zeta)} \quad (15)$$



Asymptotic approximation scheme

- ▶ Introduce “slow variation” in ζ :

$$\check{R}(\epsilon\zeta) = R(\zeta) \quad (16)$$

where $1 \gg \epsilon > 0$

- ▶ Introduce “slow coordinate” $s = \epsilon\zeta$ and

$$\check{\chi} = \sum_{n=0}^{\infty} \epsilon^n \check{\chi}_n, \quad (17)$$

where

$$\check{\chi} \in \{ \check{W}, \check{X}, \check{H}^B, \check{H}^b, \check{H}^\Phi, \check{H}^\varphi \} \quad (18)$$

N.B. Assume potentials depend on ζ through s only.



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Yields a hierarchy of Poisson and Laplace equations



Longitudinal wake potential

$$W^{\parallel}(r, \theta, u) = -\frac{1}{q_0} \int_{-\infty}^{\infty} E_z|_{ct=z-u} dz \quad (19)$$

For simplicity, assume that the source is on-axis and gaussian in
 $u = z - ct$

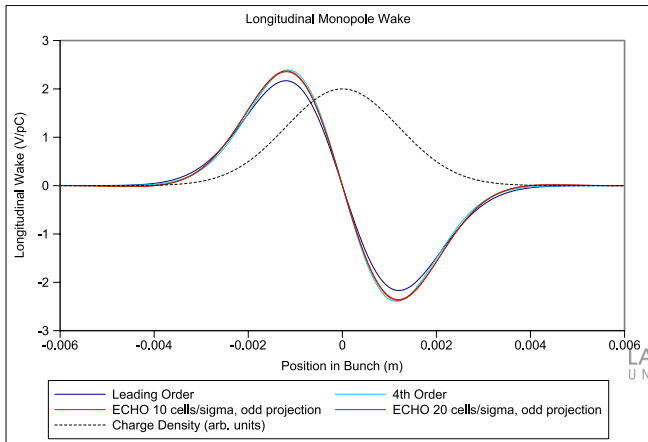


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Longitudinal wake potential : I

$$r = R(z) = 20 - 18 \exp[-z^2 / (8 \times 10^5 / l^2)], \quad \epsilon = 1 / \sqrt{8 \times 10^5} \quad (20)$$

$l = 1\text{mm}$ and z, r are measured in mm



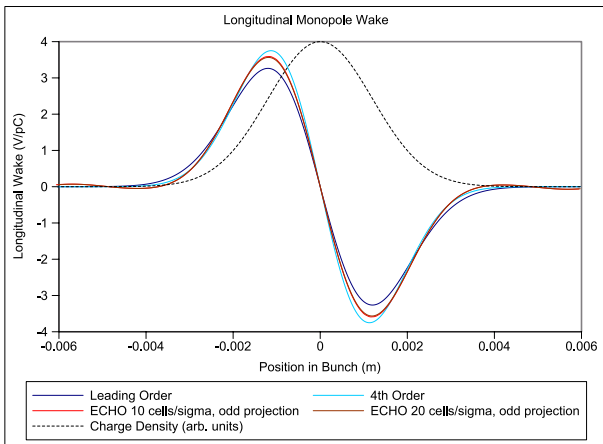


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Longitudinal wake potential : II

$$r = R(z) = 20 - 18\text{sech}(0.01z/l), \quad \epsilon = 0.01 \quad (21)$$

$l = 1\text{mm}$ and z, r are measured in mm





Impedance : on-axis harmonic charge density

$$Z_{\text{on-axis}}^{\parallel}(\omega) = Z_{1 \text{ on-axis}}^{\parallel} + Z_{2 \text{ on-axis}}^{\parallel} + Z_{4 \text{ on-axis}}^{\parallel} + Z_{6 \text{ on-axis}}^{\parallel} + \dots \quad (22)$$

where

$$Z_{1 \text{ on-axis}}^{\parallel} = \frac{1}{2\pi\epsilon_0 c} \ln \left(\frac{R_1}{R_2} \right), \quad (23)$$

$$Z_{2 \text{ on-axis}}^{\parallel} = -\frac{i\omega}{4\pi\epsilon_0 c^2} \int_{-\infty}^{\infty} R'^2 dz \quad (24)$$

$$Z_{4 \text{ on-axis}}^{\parallel} = \frac{i\omega}{96\pi\epsilon_0 c} \int_{-\infty}^{\infty} \left\{ 5R'^4 + 3(R R'')^2 - 2\frac{\omega^2}{c^2} (R^2 R'')^2 \right\} dz \quad (25)$$





Impedance : on-axis harmonic charge density

$$\begin{aligned} 4\pi\epsilon_0 c Z_{6 \text{ on-axis}}^{\parallel} = & \\ & - \frac{i\omega}{c} \int_{-\infty}^{\infty} \left\{ \frac{3}{16} (R'' R' R)^2 + \frac{11}{120} R'^6 + \frac{1}{48} (R^2 R''')^2 \right\} dz \\ & + \frac{i\omega^3}{c^3} \int_{-\infty}^{\infty} \left\{ \frac{11}{256} (R^3 R''')^2 - \frac{1}{6} (R^2 R' R'')^2 - \frac{73}{768} R^5 R''^3 \right\} dz \\ & + \frac{i\omega^5}{c^5} \int_{-\infty}^{\infty} \left\{ \frac{19}{160} (R^3 R' R'')^2 + \frac{73}{1920} R^7 R''^3 - \frac{19}{1920} (R''' R^4)^2 \right\} dz \end{aligned} \quad (26)$$

- ▶ Similar integrals obtained for $Z^{\perp}(\omega)$



Optimal geometry

Stationary variations of an impedance

$$Z[R] = \int_{z_1}^{z_2} \lambda(R, R', R'', R''') dz \quad (27)$$

yield a BVP for an optimal geometry.

$$\begin{aligned} 0 = \delta Z = & \int_{z_1}^{z_2} \left(\frac{\partial \lambda}{\partial R} - \frac{d}{dz} \frac{\partial \lambda}{\partial R'} + \frac{d^2 \partial \lambda}{dz^2 \partial R''} - \frac{d^3 \partial \lambda}{dz^3 \partial R'''} \right) \delta R dz \\ & + \left(\frac{\partial \lambda}{\partial R''} - \frac{d}{dz} \frac{\partial \lambda}{\partial R'''} \right) \delta R' \Big|_{z_1}^{z_2} \\ & + \frac{\partial \lambda}{\partial R'''} \delta R'' \Big|_{z_1}^{z_2} \end{aligned} \quad (28)$$



Optimal geometry

Hence, solve the ODE

$$\frac{\partial \lambda}{\partial R} - \frac{d}{dz} \frac{\partial \lambda}{\partial R'} + \frac{d^2 \partial \lambda}{dz^2 \partial R''} - \frac{d^3 \partial \lambda}{dz^3 \partial R'''} = 0, \quad (29)$$

subject to the natural BCs

$$\left(\frac{\partial \lambda}{\partial R''} - \frac{d}{dz} \frac{\partial \lambda}{\partial R'''} \right) \Big|_{z_1, z_2} = 0, \quad (30)$$

$$\frac{\partial \lambda}{\partial R'''} \Big|_{z_1, z_2} = 0 \quad (31)$$



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Optimal geometry

An optimal geometry (w.r.t. longitudinal impedance) has a linear profile, $R(z) = az + b$, independent of the source frequency ω



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- ▶ 2nd order unaffected by 4th order and 6th order corrections



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- ▶ 2nd order unaffected by 4th order and 6th order corrections
- ▶ Does this hold to all orders?
- ▶ (optimal geometry w.r.t. transverse impedance is frequency dependent)



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Further directions



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Further directions

- ▶ Resistive waveguide



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Further directions

- ▶ Resistive waveguide
- ▶ non-circular cross-sections



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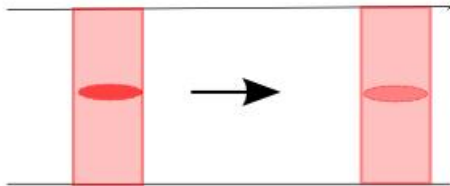
Further directions

- ▶ Resistive waveguide
- ▶ non-circular cross-sections
- ▶ Propagating modes missing



Further directions

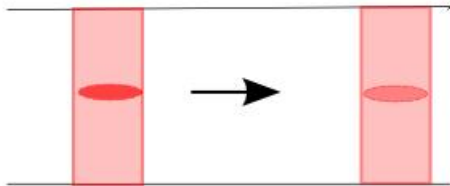
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- ▶ But sharp corners lead to wave emission, propagation and diffraction
 - ▶ \Rightarrow modal analysis



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Reference

- ▶ “Wake potentials and impedances of charged beams in gradually tapering structures”
DAB, DC Christie, JDA Smith, RW Tucker.
arXiv: 0906.0948 [physics.acc-ph]
(submitted)

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